View-Dependent Articulated-Body Simulation with Adaptive Forward Dynamics

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Outline

Introduction

Related Work

- Simulation Levels of Detail(SLODs) for Realtime Animation
- View-Dependent Culling Systems in Virtual Environments
- Divide and Conquer Algorithm(DCA) For Forward Dynamics
- Adaptive Forward Dynamics(AFD)
- View-dependent Forward Dynamics
- Conclusion



Physically-based character animation

- Support physical interaction between a character and its environment
- Generate a variety of physically correct motions



[SIMBICON: Simple Biped Locomotion Control, KangKang Yin et al., SIGGRAPH 2007]

[Realistic Modeling of Bird Flight Animations, Jia-chi Wu, Zoran Popović, SIGGRAPH 2003]



Physically-based character

Usually modeled as an articulated body



Articulated body = Rigid bodies + Joints



Simulation of the articulated-body dynamics

• Forward Dynamics (force → accel.)

The calculation of the acceleration response to a given applied force

• Inverse Dynamics (accel. → force)

The calculation of the force that must be applied in order to produce a given acceleration response





Optimal forward dynamics algorithms

• Their time complexities are linear in the number of joints, but...



[Continuum Crowds, Adrien T. at el., SIGGRAPH 2006]

Production constraints

"Dynamics computations should take less than 10-20 seconds per frame to make animators' lives easy"

Sunil Hadap, PDI/DreamWorks

We do need approximation techniques for large-scale dynamics simulations!



Related Work

Optimal Forward Dynamics

 Divide and Conquer Algorithm(DCA) For Forward Dynamics [Roy F., '99]

• Approximation of Dynamics

- Simulation Levels of Detail(SLODs) for Realtime Animation [Deborah C. and Jessica H., '97]
- View-Dependent Culling Systems in Virtual Environments [Stephen C. and David F., '97]
- Adaptive Forward Dynamics(AFD) [Stephane R. et al., `05]



SLODs for Real-time Animation

Simulation of simple hopping robots

- Move around a rectangular court
- Avoid collision with other objects

Three SLODs models

- Dynamic model
 - Fully simulated
- Hybrid model
 - •Kinematic(leg) + Dynamic(position)
- Point-mass model
 - •Only the position of the body simulated
 - •No motion of the leg (invisible case)

Recording of motions needed, Lower scalability to any other models



View-Dependent Culling Systems

- Simulation of dynamic objects in a virtual amusement park
- Culling dynamics
 - Do not solve dynamic equations of objects that are not visible
- Two main problems
 - Consistency

[pages.cs.wisc.edu/~schenney/research/culling]

In what state should culled objects be when the view turns back?

Completeness

Where and when will culled objects return to the view by themselves?



View-Dependent Culling Systems

Consistency



View window

Completeness





View-Dependent Culling Systems

Key observation

- The user has a snapshot of the approximate initial conditions
- Approaches to consistency problem
 - Predict from the initial conditions the states of the systems to which the view turns back
 - → Apply a different statistical model according to behavioral properties of each dynamic system

Study of the behavioral properties needed, Completeness problem not yet solved, Lower scalability to any other models



- One of the optimal solutions
- The spatial vector algebra used
 - Spatial vectors: 6D vectors that represent the linear and angular motions together
 - Simple and efficient to express the dynamic equations
- Divide and Conquer Algorithm (DCA)
 - Computations are recursively defined
 - Efficient parallel computing in multi-processor systems possible



Rigid body system model

- **Binary assembly tree**
 - Combines two subassembly trees recursively



Handles

Specified locations within a rigid body system at which external forces may be applied





Articulated-body equation









Articulated-body equation

- **Body A with m+1 handles** $\begin{bmatrix} a_1^A \\ a_2^A \end{bmatrix} = \begin{bmatrix} \Phi_1^A & \Phi_{12}^A \\ \Phi_{21}^A & \Phi_2^A \end{bmatrix} \begin{bmatrix} f_1^A \\ f_2^A \end{bmatrix} + \begin{bmatrix} b_1^A \\ b_2^A \end{bmatrix} \quad (H_{1_1}^A, H_{1_2}^A, \dots, H_{1_m}^A, H_2^A)$
- **Body B with n+1 handles** $\begin{bmatrix} a_1^B \\ a_2^B \end{bmatrix} = \begin{bmatrix} \Phi_1^B & \Phi_{12}^B \\ \Phi_{21}^B & \Phi_2^B \end{bmatrix} \begin{bmatrix} f_1^B \\ f_2^B \end{bmatrix} + \begin{bmatrix} b_1^B \\ b_2^B \end{bmatrix} \quad (H_1^B, H_{2_1}^B, H_{2_2}^B, ..., H_{2_n}^B)$
- **Body C with m+n handles** $\begin{bmatrix} a_{1}^{C} \\ a_{2}^{C} \end{bmatrix} = \begin{bmatrix} \Phi_{1}^{C} & \Phi_{12}^{C} \\ \Phi_{21}^{C} & \Phi_{2}^{C} \end{bmatrix} \begin{bmatrix} f_{1}^{A} \\ f_{2}^{B} \end{bmatrix} + \begin{bmatrix} b_{1}^{C} \\ b_{2}^{C} \end{bmatrix} \quad (H_{1_{1}}^{A}, H_{1_{2}}^{A}, ..., H_{1_{m}}^{A}, H_{2_{1}}^{B}, H_{2_{2}}^{B}, ..., H_{2_{n}}^{B})_{H_{2}} \\ \xrightarrow{H_{2}^{B}} \checkmark$



Articulated-body equation

- **Body A with m+1 handles** $\begin{bmatrix} a_1^A \\ a_2^A \end{bmatrix} = \begin{bmatrix} \Phi_1^A & \Phi_{12}^A \\ \Phi_{21}^A & \Phi_2^A \end{bmatrix} \begin{bmatrix} f_1^A \\ f_2^A \end{bmatrix} + \begin{bmatrix} b_1^A \\ b_2^A \end{bmatrix} \quad (H_{1_1}^A, H_{1_2}^A, \dots, H_{1_m}^A, H_2^A)$
- **Body B with n+1 handles** $\begin{bmatrix} a_1^B \\ a_2^B \end{bmatrix} = \begin{bmatrix} \Phi_1^B & \Phi_{12}^B \\ \Phi_{21}^B & \Phi_2^B \end{bmatrix} \begin{bmatrix} f_1^B \\ f_2^B \end{bmatrix} + \begin{bmatrix} b_1^B \\ b_2^B \end{bmatrix} \quad (H_1^B, H_{2_1}^B, H_{2_2}^B, ..., H_{2_n}^B)$
- **Body C with m+n handles** $\begin{bmatrix} a_{1}^{C} \\ a_{2}^{C} \end{bmatrix} = \begin{bmatrix} \Phi_{1}^{C} & \Phi_{12}^{C} \\ \Phi_{21}^{C} & \Phi_{2}^{C} \end{bmatrix} \begin{bmatrix} f_{1}^{A} \\ f_{2}^{B} \end{bmatrix} + \begin{bmatrix} b_{1}^{C} \\ b_{2}^{C} \end{bmatrix} \quad (H_{1_{1}}^{A}, H_{1_{2}}^{A}, ..., H_{1_{m}}^{A}, H_{2_{1}}^{B}, H_{2_{2}}^{B} ..., H_{2_{n}}^{B})_{H_{2_{n}}^{B}} \\ \xrightarrow{H_{2_{n}}^{B}} H_{2_{n}}^{B} = \begin{bmatrix} \Phi_{1}^{C} & \Phi_{12}^{C} \\ \Phi_{21}^{C} & \Phi_{2}^{C} \end{bmatrix} \begin{bmatrix} f_{1}^{A} \\ f_{2}^{B} \end{bmatrix} + \begin{bmatrix} b_{1}^{C} \\ b_{2}^{C} \end{bmatrix} \quad (H_{1_{1}}^{A}, H_{1_{2}}^{A}, ..., H_{1_{m}}^{A}, H_{2_{1}}^{B}, H_{2_{2}}^{B} ..., H_{2_{n}}^{B})_{H_{2_{n}}^{B}}$

The coefficients of C can be expressed in terms of those of A and B → Divide and Conquer Algorithm (DCA) is possible!!



Two main pass

• Main pass (\uparrow)

Inverse inertias

Bias

Inverse
inertias
$$\Phi_1^C = \Phi_1^A - \Phi_{12}^A W \Phi_{21}^A$$
$$\Phi_2^C = \Phi_2^B - \Phi_{21}^B W \Phi_{12}^B$$
$$\Phi_{21}^C = \Phi_{21}^B W \Phi_{21}^A$$
$$\Phi_{12}^C = (\Phi_{21}^C)^T$$
Bias
accelerations
$$b_1^C = b_1^A - \Phi_{12}^A \gamma$$
$$b_2^C = b_2^A + \Phi_{21}^A \gamma$$

Ses

$$\begin{bmatrix} a_{1}^{C} \\ a_{2}^{C} \end{bmatrix} = \begin{bmatrix} \Phi_{1}^{C} & \Phi_{12}^{C} \\ \Phi_{21}^{C} & \Phi_{2}^{C} \end{bmatrix} \begin{bmatrix} f_{1}^{A} \\ f_{2}^{B} \end{bmatrix} + \begin{bmatrix} b_{1}^{C} \\ b_{2}^{C} \end{bmatrix}$$

$$V = (\Phi_{2}^{A} + \Phi_{1}^{B})^{-1}$$

$$W = V - VS(S^{T}VS)^{-1}S^{T}V$$

$$W = V - VS(S^{T}VS)^{-1}S^{T}V$$

$$\beta = b_{2}^{A} - b_{1}^{A} + \dot{S}\dot{q}_{0}$$

$$\gamma = W\beta + VS(S^{T}VS)^{-1}Q$$

- S: Joint motion space
- Q : Forces applied by joint actuators
- \dot{q}_0 : Velocity of the principal joint

Back-substitution pass (↓)



• Two main passes

• Main pass (\uparrow) $\begin{vmatrix} a_1^C \\ a_2^C \end{vmatrix} = \begin{vmatrix} \Phi_1^C & \Phi_{12}^C \\ \Phi_{21}^C & \Phi_2^C \end{vmatrix} \begin{vmatrix} f_1^A \\ f_2^B \end{vmatrix} +$

Inverse inertias $\Phi_{1}^{C} = \Phi_{1}^{A} - \Phi_{12}^{A} W \Phi_{21}^{A}$ $\Phi_{2}^{C} = \Phi_{2}^{B} - \Phi_{21}^{B} W \Phi_{12}^{B}$ $\Phi_{21}^{C} = \Phi_{21}^{B} W \Phi_{21}^{A}$ $\Phi_{12}^{C} = (\Phi_{21}^{C})^{T}$

bias $b_1^C = b_1^A - \Phi_{12}^A \gamma$ accelerations $b_2^C = b_2^A + \Phi_{21}^A \gamma$

$$+\begin{bmatrix} b_1^C \\ b_2^C \end{bmatrix}$$

Back-substitution pass (↓)

Joint acceleration

$$q_0 = (S^T V S)^{-1} (Q - S^T V (\Phi_{21}^A f_1^A - \Phi_{12}^B f_2^B + \beta))$$

Kinematic constraint forces

$$f_{1}^{B} = W\Phi_{21}^{A}f_{1}^{A} - W\Phi_{12}^{B}f_{2}^{B} + \gamma$$
$$f_{2}^{A} = -f_{1}^{B}$$

$$\begin{bmatrix} a_{1}^{A} \\ a_{2}^{A} \end{bmatrix} = \begin{bmatrix} \Phi_{1}^{A} & \Phi_{12}^{A} \\ \Phi_{21}^{A} & \Phi_{2}^{A} \end{bmatrix} \begin{bmatrix} f_{1}^{A} \\ f_{2}^{A} \end{bmatrix} + \begin{bmatrix} b_{1}^{A} \\ b_{2}^{A} \end{bmatrix}$$
$$\begin{bmatrix} a_{1}^{B} \\ a_{2}^{B} \end{bmatrix} = \begin{bmatrix} \Phi_{1}^{B} & \Phi_{12}^{B} \\ \Phi_{21}^{B} & \Phi_{2}^{B} \end{bmatrix} \begin{bmatrix} f_{1}^{B} \\ f_{2}^{B} \end{bmatrix} + \begin{bmatrix} b_{1}^{B} \\ b_{2}^{B} \end{bmatrix}$$





We don't need to simulate all of the joints of an articulated body to keep its plausible dynamics!!

- a: 300 joints (5.00 ms)
- b: 100 joints (1.70 ms)
- C: 50 joints (0.70 ms)
- 20 joints (0.25 ms) d:
- 1 joints (0.02 ms) e:



Hybrid bodies

- Hybrid node: its principal joint is active (simulated) but some descendents are rigid
- Rigid node: its principal joint is inactive and all the descendents are rigid / it is a leaf





both its children A and B are rigid nodes



Adaptive joint selection

Velocity metric

Motion metrics

•Acceleration metric $\mathscr{A}(C) = \begin{bmatrix} \mathbf{f}_1^A \\ \mathbf{f}_2^B \end{bmatrix}^T \begin{bmatrix} \mathbf{\Psi}_1^C & \mathbf{\Psi}_{12}^C \\ \mathbf{\Psi}_{21}^C & \mathbf{\Psi}_{22}^C \end{bmatrix} \begin{bmatrix} \mathbf{f}_1^A \\ \mathbf{f}_2^B \end{bmatrix}$

$$\Psi^{\scriptscriptstyle C}_{\scriptscriptstyle i}, \Psi^{\scriptscriptstyle C}_{\scriptscriptstyle ij}, p^{\scriptscriptstyle C}_{\scriptscriptstyle i}, \eta^{\scriptscriptstyle C}$$

: Acceleration metric coefficients

- : Articulated body
- \dot{q}_i : Velocity of joint /
- \ddot{q}_i : Acceleration of joint *i*
- A_i, V_i : Customizable weight matrices of joint *i*

The acceleration metric value of an articulated body can be computed <u>before</u> computing its joint accelerations!!

 $+ \begin{bmatrix} \mathbf{f}_1^A \\ \mathbf{f}_2^B \end{bmatrix}^T \begin{bmatrix} \mathbf{p}_1^C \\ \mathbf{p}_2^C \end{bmatrix} + \boldsymbol{\eta}^C,$

 $\mathscr{V}(C) = \sum \dot{\mathbf{q}}_i^T \mathbf{V}_i \dot{\mathbf{q}}_i$



Adaptive joint selection



Adaptive joint selection



Adaptive joint selection



Adaptive joint selection



Adaptive joint selection



Adaptive joint selection



Adaptive joint selection



Adaptive joint selection



- How to best utilize the motion metrics to save more computation time?
- How to minimize the error metric values with a given threshold value?



Large-scale virtual world

Much occlusion Very far objects Many invisible objects



[Stephane R. et al., `05]

 How to best utilize the motion metrics to save more computation time?

Occluded bodies

 Decrease weight coefficients for occluded bodies



View-dependent joint selection

• Example: Back-substitution pass ()



View-dependent joint selection



- How to best utilize the motion metrics to save more computation time?
- Occluded bodies
 - Decrease weight coefficients for occluded bodies
- Totally invisible articulated bodies
 - Set the user-specified threshold value to zero
- Distant articulated bodies
 - Decrease the user-specified threshold value

Example

ε: threshold





How to minimize the error metric values with a given threshold value?

Threshold: 100



How to minimize the error metric values with a given threshold value?

Threshold: 100 **Global priority queue** Assembly tree

How to minimize the error metric values with a given threshold value?



How to minimize the error metric values with a given threshold value?



How to minimize the error metric values with a given threshold value?

After all...

Global priority queue

Assembly tree



The global search can minimize the global error metric value!

Conclusion

SLODs

- Hybrid kinetic/dynamic model
- Visibility culling
 - Consistency problem
 - Completeness problem
- Adaptive forward dynamics

 Control the number of simulated joints by the customizable motion metrics

- View-dependent forward dynamics
 - Effectively utilize the motion metrics with visibility info



Appendix I

Derivation of the articulated-body equation

I. Single handle

Iv = constant

$$f = \frac{d}{dt}(Iv) = Ia + (v \times^* I - Iv \times)v = Ia + v \times^* Iv$$

$$f = Ia + p \qquad (p = v \times^* Iv)$$

$$a = \Phi f + b \qquad (\Phi = I^{-1}, b = -\Phi p)$$

II. Multiple handles

$$\begin{bmatrix} \mathbf{a}_1 \\ \mathbf{a}_2 \\ \vdots \\ \mathbf{a}_m \end{bmatrix} = \begin{bmatrix} \Phi_1 & \Phi_{12} & \cdots & \Phi_{1m} \\ \Phi_{21} & \Phi_2 & \cdots & \Phi_{2m} \\ \vdots & \vdots & \ddots & \vdots \\ \Phi_{m1} & \Phi_{m2} & \cdots & \Phi_m \end{bmatrix} \begin{bmatrix} \mathbf{f}_1 \\ \mathbf{f}_2 \\ \vdots \\ \mathbf{f}_m \end{bmatrix} + \begin{bmatrix} \mathbf{b}_1 \\ \mathbf{b}_2 \\ \vdots \\ \mathbf{f}_m \end{bmatrix}$$

